



Ferromagnetic Liquid Flow due to Gravity-Aligned Stretching of an Elastic Sheet

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ABSTRACT

The flow of a ferromagnetic liquid due to gravity-aligned stretching of an elastic sheet in the presence of a magnetic dipole is considered. The fluid momentum and thermal energy equations are formulated as a six parameter problem and a numerical study is made using the shooting method based on Runge – Kutta Fehlberg and Newton Raphson methods. Extensive computation on the velocity and temperature profiles is presented for a wide range of values of the parameters. It was found that the primary effect of the magnetothermomechanical interaction is to decelerate the fluid motion as compared to the hydrodynamic case. The results have possible industrial applications in ferromagnetic liquid based systems involving stretchable materials.

Keywords: Ferromagnetic liquid; Magnetic dipole; Stretching sheet; Grashof number; Prandtl number; Shooting method.

NOMENCLATURE

A, D	positive constants	α	dimensionless distance from the origin to the center of the magnetic pole
c_f	local skin friction coefficient	β	ferrohydrodynamic interaction parameter
c_p	specific heat at constant pressure	β^*	thermal expansion coefficient
g	acceleration due to gravity	\mathcal{E}	non-dimensional Curie temperature
Gr	Grashof number	$\Theta(\xi, \eta)$	nondimensional Temperature
H	magnetic field	λ	viscous dissipation parameter
K	pyromagnetic coefficient	μ	dynamic viscosity
k	thermal conductivity	μ_0	magnetic permeability
L	characteristic length	ν	kinematic viscosity
M	magnetization	ρ	fluid density
Pr	Prandtl number	τ	shear stress at the sheet
T	temperature of the fluid	ϕ	magnetic scalar potential
T_w	temperature of the stretching sheet	(ξ, η)	nondimensional lengths
T_c	Curie temperature		
(u,v)	velocity along the x, y axes		
(U,V)	nondimensional radial and axial velocities		

1. INTRODUCTION

The study of laminar boundary layer flow and heat transfer in Newtonian and non-Newtonian fluids past a stretching sheet has been investigated extensively by many researchers due to its scientific and engineering applications. In processes such as polymer extrusion, the object on passing between two closely placed solid blocks is stretched into a liquid region. The desired mechanical properties of

the extrudate depends on the rate of cooling/heating and the rate of stretching (see Fisher E.G. 1976; Bailey R.L. 1983).

In the present problem the viscous and nonconducting ferrofluid is representative of the ambient liquid which serves the purpose of controlled heat transfer in the presence of a magnetic field.

Ferrofluids are artificially synthesized and composed

of a carrier fluid and suspended particles. These particles are small (3-5 nm), solid, magnetic, single domain and coated with a molecular layer of a dispersant. Thermal agitation keeps them suspended and the coating keeps them noncolloidal (see Rosensweig R.E. 1985; Neuringer and Rosensweig 1964).

The combined influence of thermal and magnetic field gradients on the saturated ferrofluid flowing along a flat plate was investigated by Neuringer J.L. (1966). The flow of a viscous fluid past a linearly stretching surface was considered by Crane L.J. (1970) for a Newtonian fluid. Andersson and Valnes (1998) extended Crane's problem by studying the influence of the magnetic field, due to a magnetic dipole, on a shear driven motion (flow over a stretching sheet) of a viscous non-conducting ferrofluid. It was concluded that the primary effect of the magnetic field was to decelerate the fluid motion as compared to the hydrodynamic case.

At the present time there are enumerable papers on the stretching sheet problem using different continua and considering various effects such as non-Newtonian characteristics, radiation, and magnetic field and so on. The above discussions can be found in Abel *et al.* 2008, 2009a, 2009b, 2009c, 2009d, 2011; Andersson 1998, 1992, 2006; Cortell 2010, 2008, 2007a, 2007b, 2006; Dandapat 2011, 2010, 2007; Dulal Pal 2010a, 2010b; Siddheshwar and Mahabaleshwar 2005; Hayat *et al.* 2010a, 2010b; Abbas *et al.* 2010; Wang C.Y. 2007; Hamad 2007; Arnold *et al.* 2010; Seddeek 2007; Prasad *et al.* 2010; Magyari and Keller 2006; Van Gorder and Vajravelu 2010; Vajravelu and Cannon 2006; Abdoul and Ghotbi 2009; Tzirtzilakis and Kafoussias 2003 and the references there in.

In many of the physical situation the sheet may be stretched vertically, rather than horizontally, into the ambient liquid. In this case the liquid flow and the heat transfer characteristics are determined by the motion of the stretching sheet and the buoyant force. There are no studies in literature concerning the flow and heat transfer in a ferrofluid due to a vertical stretching sheet in the presence of external magnetic field. This paper aims at studying the same using two different types of boundary heating, namely, prescribed surface temperature (PST) and prescribed surface heat flux (PHF). Shooting method based on Runge-Kutta-Fehlberg and Newton Raphson schemes is used in arriving at the numerical solution of the proposed problem.

2. MATHEMATICAL FORMULATION

Consider a steady two-dimensional flow of an incompressible, viscous and electrically non conducting ferrofluid driven by an impermeable sheet in the vertical direction. By applying two equal and opposite forces along the direction of gravity which is taken as the x-axis, and y-axis in a direction normal to the flow, the sheet is stretched with a velocity $u_w(x)$ which is proportional to the distance from the origin. A magnetic dipole is located some distance from the sheet. The centre of

the dipole lies on the y-axis at a distance 'a' from the x-axis and whose magnetic field points in the positive x-direction giving rise to a magnetic field of sufficient strength to saturate the ferrofluid. The stretching sheet is kept at a fixed temperature T_w below the Curie temperature T_c , while the fluid elements far away from the sheet are assumed to be at temperature $T = T_c$ and hence incapable of being magnetized until they begin to cool upon entering the thermal boundary layer adjacent to the sheet.

The boundary layer equations governing the flow and heat transfer in a ferrofluid are as follows,

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial v}{\partial y} = \frac{\mu}{\rho} \frac{\partial^2 u}{\partial y^2} + \frac{\mu_0}{\rho} M \frac{\partial H}{\partial x} + g \beta^* (T_c - T) \tag{2}$$

$$\rho c_p \left(u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) + \mu_0 T \frac{\partial M}{\partial T} \left(u \frac{\partial H}{\partial x} + v \frac{\partial H}{\partial y} \right) = k \frac{\partial^2 T}{\partial y^2} + \mu \left(\frac{\partial u}{\partial y} \right)^2 + 2\mu \left(\frac{\partial v}{\partial y} \right)^2 \tag{3}$$

where u and v are the velocity components along x and y directions respectively, ρ is the fluid density,

μ the dynamic viscosity, $\nu = \frac{\mu}{\rho}$ the kinematic

viscosity, C_p specific heat at constant pressure, k the thermal conductivity, g the acceleration due to gravity, β^* representing the coefficient of thermal expansion, μ_0 the magnetic permeability, M the magnetization, H the magnetic field, T the temperature of the fluid.

The assumed boundary conditions for solving the above equations are:

$$\left. \begin{aligned} u = cx, v = 0, \\ T = T_w = T_c - A \left(\frac{x}{L} \right) \quad \text{in PST} \\ -k \frac{\partial T}{\partial y} = q_w = D \left(\frac{x}{L} \right) \quad \text{in PHF} \end{aligned} \right\} \text{at } y = 0 \tag{4}$$

$$u \rightarrow 0, \quad T \rightarrow T_c \quad \text{as } y \rightarrow \infty \tag{5}$$

where k is the thermal conductivity of the fluid. A and D are positive constants and $L = \sqrt{\frac{\nu}{c}}$ is the characteristic length. The flow of ferrofluid is affected by the magnetic field due to the magnetic dipole whose magnetic scalar potential is given by:

$$\phi = \frac{\alpha'}{2\pi} \left(\frac{x}{x^2 + (y+a)^2} \right), \quad (6)$$

where α' is the dipole moment per unit length.

The magnetic field H has the components

$$H_x = -\frac{\partial\phi}{\partial x} = \frac{\alpha'}{2\pi} \frac{x^2 - (y+a)^2}{(x^2 + (y+a)^2)^2} \quad (7)$$

$$H_y = -\frac{\partial\phi}{\partial y} = \frac{\alpha'}{2\pi} \frac{2x(y+a)}{(x^2 + (y+a)^2)^2} \quad (8)$$

Since the magnetic body force is proportional to the gradient of the magnitude of \vec{H} , we obtain:

$$H = \left[\left(\frac{\partial\phi}{\partial x} \right)^2 + \left(\frac{\partial\phi}{\partial y} \right)^2 \right]^{\frac{1}{2}} \quad (9)$$

$$\frac{\partial H}{\partial x} = -\frac{\alpha'}{2\pi} \left(\frac{2x}{(y+a)^4} \right), \quad (10)$$

$$\frac{\partial H}{\partial y} = \frac{\alpha'}{2\pi} \left(\frac{-2}{(y+a)^3} + \frac{4x^2}{(y+a)^5} \right)$$

Variation of magnetization M with temperature T is approximated by a linear equation

$$M = K (T_c - T) \quad (11)$$

where K is the *pyromagnetic* coefficient.

3. SOLUTION PROCEDURE

We now introduce the non - dimensional variables as assumed by Andersson (1998).

$$(\xi, \eta) = \left(\frac{c}{v} \right)^{\frac{1}{2}} (x, y), \quad (U, V) = \frac{(u, v)}{\sqrt{cv}}, \quad (12)$$

$$\theta(\xi, \eta) = \frac{T_c - T}{T_c - T_w} = \begin{cases} \theta_1(\eta) + \xi^2 \theta_2(\eta) & \text{in PST case} \\ \phi_1(\eta) + \xi^2 \phi_2(\eta) & \text{in PHF case} \end{cases} \quad (13)$$

Where $T_c - T_w = A \left(\frac{x}{L} \right)$ in PST case,

$$T_c - T_w = \frac{DL}{k} \left(\frac{x}{L} \right) \text{ in PHF case.}$$

The boundary layer equations 1-3 on using 10-13 takes the following form:

$$\frac{\partial U}{\partial \xi} + \frac{\partial V}{\partial \eta} = 0 \quad (14)$$

$$U \frac{\partial U}{\partial \xi} + V \frac{\partial U}{\partial \eta} = \frac{\partial^2 U}{\partial \eta^2} - \frac{2\beta\xi}{(\eta+4)^4} (\theta_1 + \xi^2 \theta_2) + Gr\xi (\theta_1 + \xi^2 \theta_2) \quad (15)$$

$$\begin{aligned} &Pr [2U\xi\theta_2 + V(\theta_1 + \xi^2\theta_2)] \\ &+ \beta\lambda(\varepsilon - \theta_1 + \xi^2\theta_2) \left[\frac{-2\xi U}{(\eta+\alpha)^4} - \frac{2V}{(\eta+\alpha)^3} + \frac{4\xi^2 V}{(\eta+\alpha)^5} \right] \\ &= \theta_1' + \xi^2 \theta_2' - \lambda \left(\frac{\partial U}{\partial \eta} \right)^2 - 2\lambda \left(\frac{\partial V}{\partial \eta} \right)^2 \end{aligned} \quad (16)$$

The boundary conditions, given by Eq. (4), now takes the form:

$$\left. \begin{aligned} U(\xi, 0) &= \xi, & V(\xi, 0) &= 0, \\ \theta_1(\xi, 0) &= 1, & \theta_2(\xi, 0) &= 0, & \text{(PST),} \\ \phi_1(\xi, 0) &= -1, & \phi_2(\xi, 0) &= 0, & \text{(PHF),} \\ U(\xi, \infty) &\rightarrow 0, & \theta(\xi, \infty) &\rightarrow 0 \end{aligned} \right\} \quad (17)$$

Introducing the stream function $\psi(\xi, \eta) = \xi f(\eta)$ that satisfies the continuity equation in the dimensionless form 14, we obtain:

$$U = \frac{\partial\psi}{\partial\eta} = \xi f'(\eta), \quad V = \frac{\partial\psi}{\partial\xi} = -f(\eta), \quad (18)$$

where the prime denotes differentiation with respect to η . On using Eq. (10), Eq. (12) and Eq. (18) in Eq. (15) and Eq. (16), we obtain the following boundary value problem

(i) PST

$$f''' + ff'' - (f')^2 - \frac{2\beta\theta_1}{(\eta+\alpha)^4} + Gr\theta_1 = 0 \quad (19)$$

$$\begin{aligned} &\theta_1'' + Pr (f\theta_1' - f'\theta_1) \\ &+ \frac{2\beta f\lambda}{(\eta+\alpha)^3} (\theta_1 - \varepsilon) - 2\lambda(f')^2 = 0, \end{aligned} \quad (20)$$

$$\theta_2'' - \lambda(f')^2 - Pr(3f'\theta_2 - f\theta_2') + \frac{2\lambda\beta f\theta_2}{(\eta+\alpha)^3} \quad (21)$$

$$-\lambda\beta(\theta_1 - \varepsilon) \left[\frac{2f'}{(\eta+\alpha)^4} + \frac{4f}{(\eta+\alpha)^5} \right] = 0,$$

$$f = 0, \quad f' = 1, \quad \theta_1 = 1, \quad \theta_2 = 0 \quad \text{at } \eta = 0 \quad (22)$$

$$f' \rightarrow 0, \quad \theta_1 \rightarrow 0, \quad \theta_2 \rightarrow 0 \quad \text{as } \eta \rightarrow \infty \quad (23)$$

(ii) PHF

$$f'''' + ff'' - (f')^2 - \frac{2\beta\phi_1}{(\eta + \alpha)^4} + Gr\phi_1 = 0 \quad (24)$$

$$\phi_1'' + Pr(f\phi_1' - f'\phi_1) + \frac{2\beta f \lambda}{(\eta + \alpha)^3} (\phi_1 - \varepsilon) - 2\lambda f'^2 = 0 \quad (25)$$

$$\phi_2'' - \lambda(f')^2 - Pr(3f'\phi_2 - f\phi_2') + \frac{2\lambda\beta f \phi_2}{(\eta + \alpha)^3} - \lambda\beta(\phi_1 - \varepsilon) \left[\frac{2f'}{(\eta + \alpha)^2} + \frac{4f}{(\eta + \alpha)^3} \right] = 0 \quad (26)$$

$$f = 0, f' = 1, \phi_1 = -1, \phi_2 = 0 \text{ at } \eta = 0 \quad (27)$$

$$f \rightarrow 0, \phi_1 \rightarrow 0, \phi_2 \rightarrow 0 \text{ as } \eta \rightarrow \infty \quad (28)$$

The six dimensionless parameters, which appear explicitly in the transformed problem, are the Prandtl number Pr , the viscous dissipation parameter λ , the dimensionless Curie temperature ε , the ferrohydrodynamic interaction parameter β , the Grashof number Gr and the dimensionless distance α from the origin to the center of the magnetic pole, defined respectively as

$$Pr = \frac{\mu C_p}{k}, \lambda = \frac{c\mu^2}{\rho k(T_c - T_w)}, \varepsilon = \frac{T_c}{T_c - T_w}, \beta = \frac{\alpha \rho}{2\pi\mu^2} \mu_0 K(T_c - T_w), Gr = \frac{g\beta^2 A}{c^2 L}, \alpha = \left(\frac{c\rho a^2}{\mu} \right)^{\frac{1}{2}} \quad (29)$$

The local skin friction coefficient C_f , which is a dimensionless form of the shear stress τ at the sheet is given by:

$$C_f = \frac{-2\tau_w}{\rho(cx)^2} = -2f''(0) Re_x^{-\frac{1}{2}} \quad (30)$$

In the PST case we are fixing the surface temperature and hence we calculate the local heat flux as follows,

$$Nu_x = -Re_x^{\frac{1}{2}} [\theta_1'(0) + \xi^2 \theta_2'(0)] \quad (31)$$

In the PHF case we are fixing the surface heat flux and hence we compute the surface temperature as follows,

$$Tw = Tc - \frac{DL}{k} \left(\frac{x}{L} \right) [\phi_1(0) + \xi^2 \phi_2(0)] \quad (32)$$

3.1 Method of Solution:

The three coupled differential equations (19) to (21) subject to the boundary conditions (22) and (23) constitute a non - linear two - point boundary value problem, which is solved by means of a standard shooting technique. The higher order ordinary differential equations are formulated as first order equations and the resulting set of seven first order equations can be integrated as an initial value problem using the adaptive stepping Runge-Kutta-Fehlberg (RKF45) method. The trial values of $f'(0), \theta_1(0), \theta_2(0)$ were adjusted iteratively by Newton Raphson's method to assure a quadratic convergence of the iterations required in order to fulfill the right end boundary conditions. The initial value problem to be solved are given below

3.2 Initial Value Problem-1 (IVP-1)

$$\left. \begin{aligned} \frac{dy_1}{dx} &= y_2, \\ \frac{dy_2}{dx} &= y_3, \\ \frac{dy_3}{dx} &= y_2^2 - y_1 y_3 + \frac{2\beta y_4}{(\eta + \alpha)^4} - Gr y_4, \\ \frac{dy_4}{dx} &= y_5, \\ \frac{dy_5}{dx} &= -Pr y_1 y_5 - \frac{2\beta \lambda y_1 (y_4 - \varepsilon)}{(\eta + \alpha)^3} + 2\lambda y_2^2, \\ \frac{dy_6}{dx} &= y_7, \\ \frac{dy_7}{dx} &= \lambda y_3^2 - Pr(y_1 y_7 - 2y_2 y_6) - \frac{2\lambda \beta y_1 y_6}{(\eta + \alpha)^3} \\ &+ \lambda \beta (y_4 - \varepsilon) \left[\frac{2y_2}{(\eta + \alpha)^4} + \frac{4y_1}{(\eta + \alpha)^3} \right], \end{aligned} \right\} \quad (33)$$

with the initial conditions:

$$y_1(0)=0, y_2(0) = 1, y_3(0) = a_0, y_4(0) = 1, y_5(0) = b, y_6(0) = 0, y_7(0) = c_0 \quad (34)$$

We need to solve a sequence of initial value problems as above so that the end boundary values thus obtained numerically match upto a desired degree of tolerance with the boundary values at ∞ given in the problem. Now the problem is to find a_0, b_0, c_0 such that:

$$\begin{aligned} F_1(a_0, b_0, c_0) &= f'(\infty, a_0, b_0, c_0) - f'(\infty) = y_2(\infty, a_0, b_0, c_0) - y_2(\infty), \\ F_2(a_0, b_0, c_0) &= \theta_1(\infty, a_0, b_0, c_0) - \theta_1(\infty) = y_4(\infty, a_0, b_0, c_0) - y_4(\infty), \end{aligned}$$

$$F_3(a_0, b_0, c_0) = \theta_2(\infty, a_0, b_0, c_0) - \theta_2(\infty) = y_6(\infty, a_0, b_0, c_0) - y_6(\infty). \quad (35)$$

These are three nonlinear equations in a, b, and c which are solved by the Newton-Raphson method. This method for finding roots of non-linear equations, with a_0, b_0 and c_0 as the initial values, yields the following iterative scheme:

$$\begin{pmatrix} a_{n+1} \\ b_{n+1} \\ c_{n+1} \end{pmatrix} = \begin{pmatrix} a_n \\ b_n \\ c_n \end{pmatrix} + \begin{pmatrix} \frac{\partial F_1}{\partial a} & \frac{\partial F_1}{\partial b} & \frac{\partial F_1}{\partial c} \\ \frac{\partial F_2}{\partial a} & \frac{\partial F_2}{\partial b} & \frac{\partial F_2}{\partial c} \\ \frac{\partial F_3}{\partial a} & \frac{\partial F_3}{\partial b} & \frac{\partial F_3}{\partial c} \end{pmatrix}^{-1} \begin{pmatrix} F_1 \\ F_2 \\ F_3 \end{pmatrix} \quad (a_n, b_n, c_n)$$

$$(n = 0, 1, 2, \dots). \quad (36)$$

To implement Newton-Raphson method, the nine partial derivatives of F_1, F_2 and F_3 with respect to a, b and c are required. By differentiating the IVP 1 of Eq. (33) and Eq. (34), with respect to a and setting

$Y_i = \frac{\partial y_i}{\partial a}$, the second initial value problem (IVP-2) is obtained.

3.3 Initial Value Problem-2 (IVP-2)

$$\begin{aligned} \frac{dY_1}{dx} &= Y_2 \\ \frac{dY_2}{dx} &= Y_3 \\ \frac{dY_3}{dx} &= 2y_2Y_2 - y_1Y_3 - Y_1Y_3 - GrY_4 + \frac{2\beta Y_4}{(\eta + \alpha)^4} \\ \frac{dY_4}{dx} &= Y_5 \\ \frac{dY_5}{dx} &= -Pr y_1Y_5 - Pr Y_1Y_5 - \frac{2\beta\lambda}{(\eta + \alpha)^3} [Y_1(y_4 - \varepsilon) + y_1Y_4] \\ &\quad + 4\lambda y_2Y_2 \\ \frac{dY_6}{dx} &= Y_7 \\ \frac{dY_7}{dx} &= 2\lambda y_3Y_3 - Pr [Y_1y_7 + y_1Y_7 - 2y_2Y_6 - 2Y_2y_6] \\ &\quad - \frac{2\lambda\beta}{(\eta + \alpha)^3} [y_1Y_6 + Y_1y_6] + \lambda\beta Y_4 \left[\frac{2y_2}{(x + \alpha)^4} + \frac{4y_1}{(x + \alpha)^5} \right] \\ &\quad + \lambda\beta(y_4 - \varepsilon) \left[\frac{2Y_2}{(x + \alpha)^4} + \frac{4Y_1}{(x + \alpha)^5} \right] \end{aligned} \quad (37)$$

with the initial conditions,

$$Y_1(0) = 0; Y_2(0) = 0; Y_3(0) = 1; Y_4(0) = 0;$$

$$Y_5(0) = 0; Y_6(0) = 0; Y_7(0) = 0. \quad (38)$$

Similarly IVP-3, IVP-4 are obtained by differentiating IVP-1 with respect to b and c respectively. Thus three additional initial value problems IVP-2, IVP-3 and IVP-4 known as the variational equations in literature, are obtained and solved using variable stepping RKF45 method.

4. RESULTS AND DISCUSSION

An analysis is carried out to study the effect of magnetic field on the flow of the ferromagnetic liquid due to a vertically stretched sheet. Heat transfer is studied using two different boundary heating, namely, PST and PHF. With the aid of similarity transformations the partial differential equations governing the flow and heat transfer are converted into a set of non-linear coupled ordinary differential equations. The resulting problem is a boundary value one and the same is solved using shooting technique based on RKF45 and NR methods. The numerical results are shown in the form of graphs from Figs. 2 to 7. The skin friction coefficient is tabulated in Table 1 for a wide range of values of the governing parameters.

Figure (2) shows the effect of ferrohydrodynamic interaction parameter β on velocity profiles $f'(\eta)$ for PST and PHF cases. From these plots it is evident that increasing values of β results in flattening of $f'(\eta)$. The transverse contraction of the velocity boundary layer is due to the applied magnetic field, which produces considerable opposition to the motion.

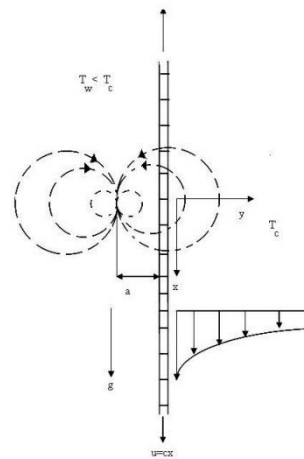


Fig. 1. Schematic representation of flow configuration (broken lines represent the magnetic field)

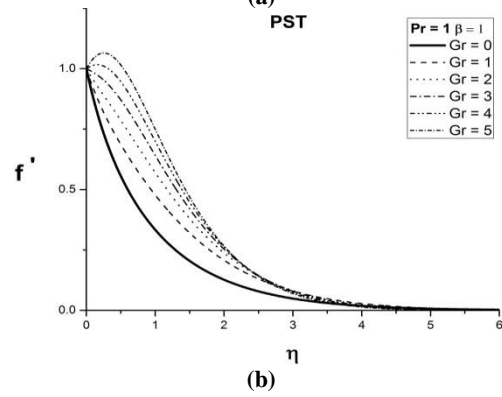
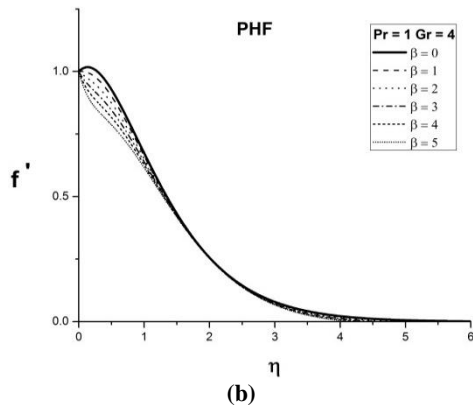
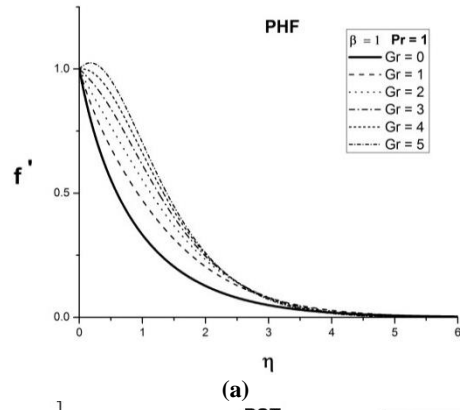
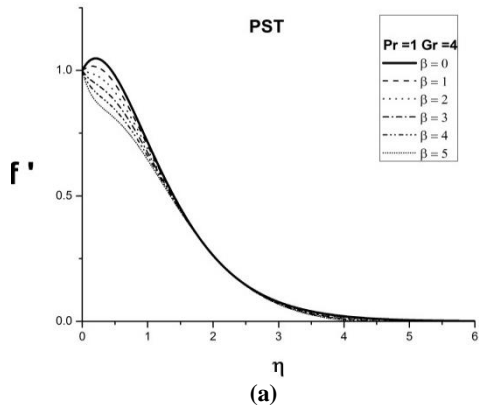


Fig. 2. Effect of ferrohydrodynamic interaction parameter β on velocity profile in PST and PHF with $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

Fig. 4. Effect of Grashof number Gr on velocity profile in PST and PHF $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

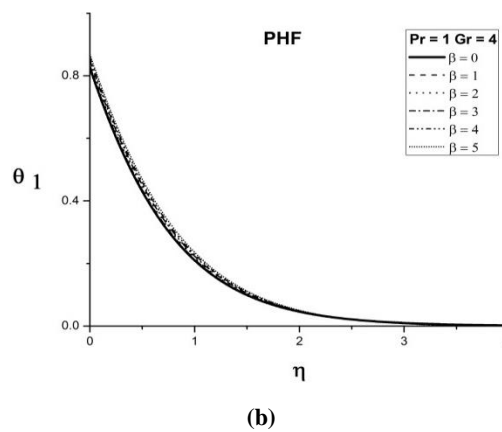
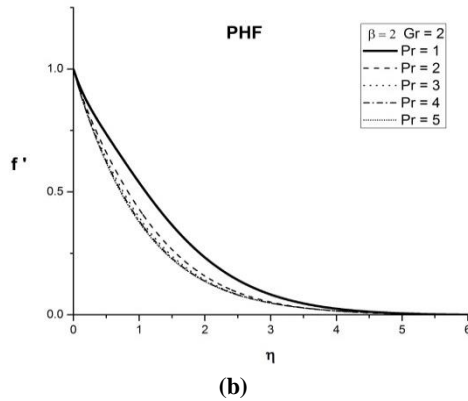
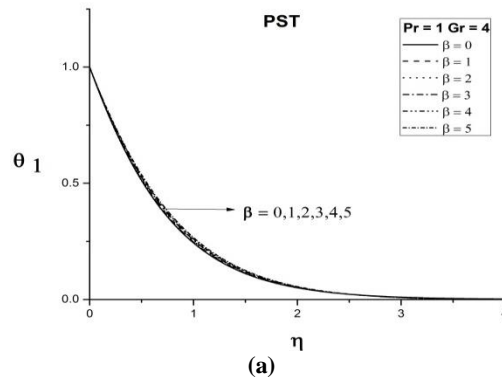
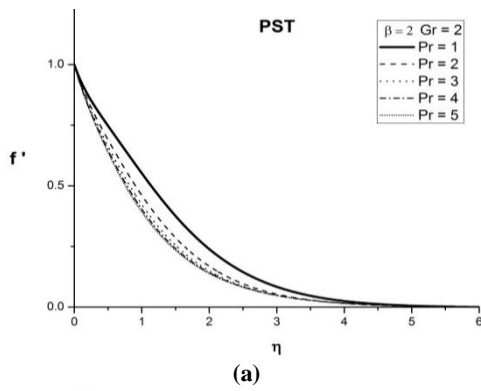


Fig. 3. Effect of Prandtl number Pr on velocity profile in PST and PHF with $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

Fig. 5. Effect of ferrohydrodynamic interaction parameter β on temperature profile in PST and PHF with $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

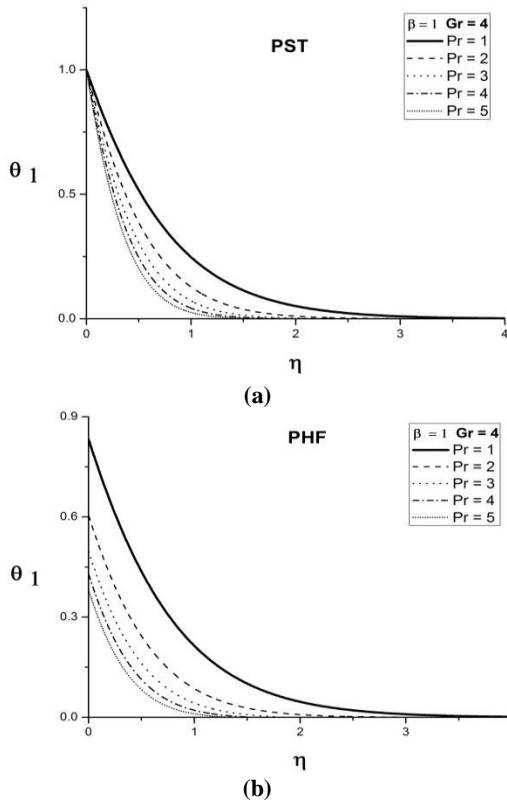


Fig. 6. Effect of Prandtl number Pr on temperature profile in PST and PHF with $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

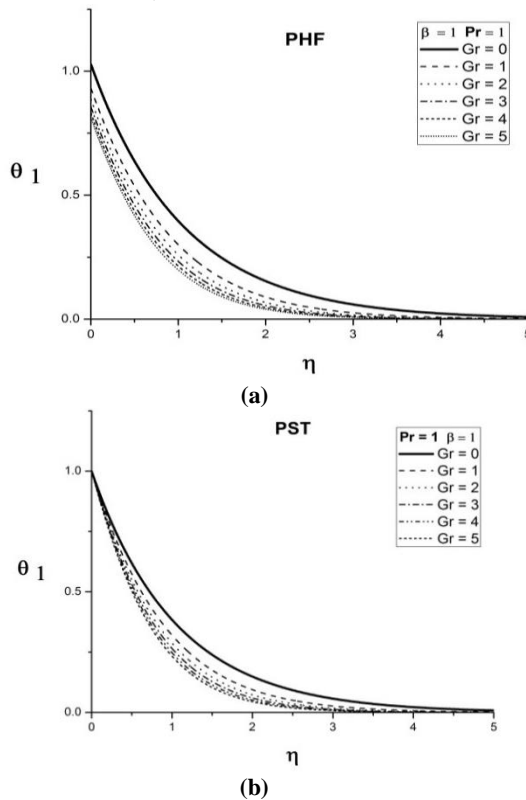


Fig. 7. Effect of Grashof number Gr on temperature profile in PST and PHF with $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

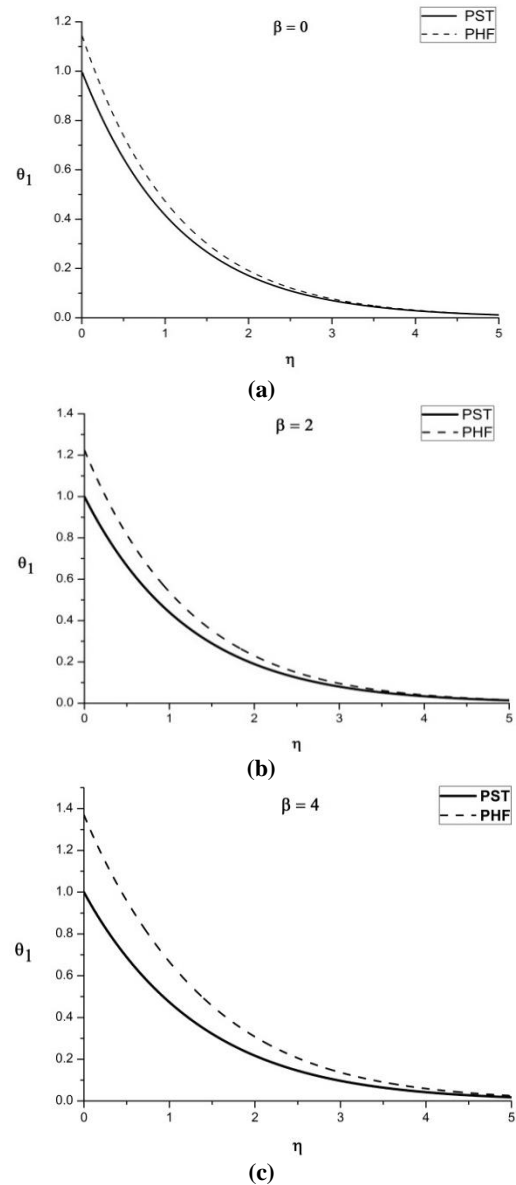


Fig. 8. Comparison of heat transfer in two boundary conditions PST and PHF when β is varied with $\alpha = 1$, $\varepsilon = 2$ and $\lambda = 0.01$

From Fig. 3 which illustrates the effect of Pr on the velocity profiles it is clear that increasing values of Pr reduces the horizontal velocity profiles in both PST and PHF cases. The Prandtl number is the ratio of two diffusivities, diffusivity of momentum and vorticity and that of the heat. At high Prandtl number the fluid is very viscous and the velocity is reduced.

The effect of Grashof number Gr on the horizontal velocity profiles is shown in Fig. 4 for the cases of PST and PHF. The Grashof number highlights the significance of convection in controlling the axial velocity. These plots indicate that the momentum boundary layer thickness increases with the increasing values of Gr , enabling the fluid to flow freely. The buoyancy force evolved as a consequence of the cooling of the vertical stretching sheet acts like a favourable pressure gradient

accelerating the fluid in the boundary layer region. It also indicates the relative importance of inertia to viscous forces. When Gr is large the domination of advection over conduction always occurs simultaneously with dominance of inertial forces over viscous forces. It can also be interpreted as that the flow will have a boundary layer character.

Figure (5) shows the effect of β on temperature profiles. As β increases the skin friction is increased which enhances the heat transfer. The same effect is reiterated in Fig. 5. A number of striking phenomena are exhibited by the magnetic fluid in response to the impressed magnetic fields. These responses include the normal field instability due to which a pattern of spikes appears on the fluid surface, enhanced convective cooling in ferrofluids having a temperature dependent magnetic moment, unusual buoyancy relationships, such as the self-levitation of an immersed magnet. The parameter β has a regulating effect on the fluid as it regulates

the velocity of the motion. This happens only at the lower values of β , but at higher values some unrealistic patterns are observed.

Figure (6) highlights the effect of thermal diffusivity parameter Pr on heat transfer. It is clear from this figure that the fluid with lesser Prandtl number is effective in controlling the heat transfer. The effect of Grashof number on heat transfer is same as that of Pr as can be seen from Fig. 7. Here we note that for Gr = 0 recovers the results of horizontal stretching sheet problem.

The skin friction coefficient is tabulated in Table 1 for various values of β , Pr and Gr. This table highlights the same effects of the parameters that we have discussed through figures. The skin friction is increased in presence of magnetic field ($\beta = 2$) as compared to the case of absence of magnetic field ($\beta = 0$) that is, β dominates in controlling the heat transfer as compared to other parameters.

Table 1 Values of $-f''(0)$ for different values of Gr and Pr in the absence / presence of ferromagnetism for PST and PHF

		$-f''(0)$			
Gr	Pr	PST		PHF	
		$\beta = 0$	$\beta = 2$	$\beta = 0$	$\beta = 2$
1	2	0.597198	1.264163	0.590702	1.280894
		0.233778	0.878759	0.252027	0.878351
		-0.106231	0.523613	-0.049035	0.537847
		-0.429651	0.188691	-0.325007	0.233937
		-0.740288	-0.131168	-0.582449	-0.044760
		-1.040571	-0.439099	-0.825365	-0.304578
2	1	0.062698	0.751592	-0.209880	0.686542
	2	0.233778	0.878759	0.252027	0.878351
	3	0.330682	0.984821	0.458720	0.952642
	4	0.396045	0.984821	0.576737	0.988155
	5	0.444270	1.012052	0.652899	1.007067
	6	0.481881	1.031515	0.706001	1.017839

From the Fig. 8 it is clear that the thermal boundary layer thickness in PHF case exceeds the PST case showing that more heat is diffused away into the system. Hence the PHF boundary conditions are better suited for proper cooling of the sheet. As mentioned earlier the desired properties of the extrudate depend on the rate of cooling. For applications where in the better cooling rate is required the PHF boundary condition can be made use.

5. CONCLUSIONS

The following inference is arrived at from the results that we have discussed in the previous section.

1. The ferrohydrodynamic interaction parameter β has a significant say in the control of flow and heat transfer of the ferrofluid. It should be kept at minimum.

2. Grashof and Prandtl numbers assists flow thereby reducing heat transfer hence these parameters also must be at their minimum for effective cooling.

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